



A physical analysis of the factors which influence the shape of a B-H loop has already been made.<sup>1</sup> A criterion for a square B-H loop was found to be  $H_n \geq H_c$  where  $H_n$  is the field strength at which new domains of reverse magnetization are formed. (Only the  $H_n$  of those reverse domains which are created within the hysteresis cycle directly effect the B-H loop.) The analysis of the lattice imperfections at which reverse domains may be nucleated showed that although granular inclusions strongly influence the coercivity of a material, they do not act as nucleating centers for mobile domain walls. Rather grain boundaries and lamellar precipitates, if present, were found to be the significant nucleation centers for mobile domains of reverse magnetization. The critical field strength for reverse-domain creation at these lattice imperfections is

$$H_n \propto (\sigma_w - \alpha \omega^*{}^2)$$

where  $\alpha$  is a constant which depends upon the geometry of the created domain and the distance between internal planes of magnetic-pole surface density  $\omega^*$ . The energy per unit area of 180° Bloch wall is  $\sigma_w$ . At a grain boundary  $\omega^* = I_s (\cos \theta_1 - \cos \theta_2)$  where  $\theta_1$  and  $\theta_2$  are the angles the magnetization vector in two neighboring grains makes with the normal to their common boundary. At a lamellar precipitate  $\omega^* = \omega_p^* = (I_s \cos \theta_s - I_p \cos \theta_p)$  where  $I_p$  is the spontaneous magnetization of the precipitate. If a material has a large magnetostriction coefficient,  $(\cos \theta_1 - \cos \theta_2)$  will be stress sensitive, and the shape of the B-H loop will be stress sensitive. If lamellar precipitates are present, however,  $\omega_p^*$  will be relatively insensitive to stress.

Currently the most successful materials for memory cores come from the magnesium-manganese-ferrite system. These materials, if judged by the sensitivity of the B-H loop to externally applied stress, have relatively low magnetostrictive constants. The squareness of the B-H loop in these materials is not, therefore, attributed to internal stresses. It is rather believed due to a value of  $\sigma_w / \omega^*{}^2 > \alpha$ , or to a positive  $H_n$ . Although there is no grain orientation to reduce  $(\cos \theta_1 - \cos \theta_2)$ , the spontaneous magnetization in these materials is an order of magnitude smaller than in iron whereas  $\sigma_w \propto \sqrt{KA}$  is as large as in iron. The anisotropy constant K will be sensitive to the chemical composition of the material. The exchange parameter A will

1. J. B. Goodenough and N. Menyuk, "A Theory of Domain Creation, Coercive Force, and Flux Reversal in Polycrystalline Ferromagnets", Lincoln Technical Report T-40 (1953).

probably be less sensitive to small variations in chemical composition.

It is of interest to predict, in the light of this analysis, in which compositional areas of the  $\text{MgO-Fe}_2\text{O}_3\text{-MnO}$  diagram the most satisfactory memory cores are to be found. In Section II an analysis is made of the mechanism of precipitation of lamellar  $2\text{MO}\cdot\text{MnO}_2$ . The symbol M stands for a bivalent metal cation. In those compositional regions in which extensive lamellar precipitation occurs,  $H_n < 0$  and the B-H loop is not square. In Section III an analysis is made of those compositional regions in which lamellar precipitation of  $2\text{MO}\cdot\text{MnO}_2$  may be expected to occur. It is also shown how this region will change its area under different firing atmospheres. In Section IV there is a comparison of these predictions with the results of a preliminary experimental investigation of this system.

## II. Precipitation of $\text{Mn}_3\text{O}_4$ on $\{101\}$ Planes

Hausmannite ( $\text{Mn}_3\text{O}_4$ ) has a tetragonal spinel structure with  $c/a = 1.16$ .<sup>2</sup> Its electrical conductivity is  $10^8 - 10^9$  smaller than in  $\text{Fe}_3\text{O}_4$ .<sup>3</sup> Verwey and his co-workers have proposed that  $\text{Mn}_3\text{O}_4$  consists of  $2\text{MnO}\cdot\text{MnO}_2$  rather than  $\text{MnOMn}_2\text{O}_3$  and that the spinel is inverse with the  $\text{Mn}^{+4}$  and  $\text{Mn}^{+2}$  ions so ordered in the octahedral sites as to occupy alternate planes parallel to the c axis.<sup>4</sup> Such ordering is similar to that found in magnetite ( $\text{Fe}_3\text{O}_4$ ) below  $120^\circ \text{K}$ .<sup>5</sup> The suggestion was supported by a calculation of the Madelung-energy gain due to ordering. Further support for this hypothesis is given by Goodenough and Loeb<sup>6</sup> who also propose that  $\gamma\text{-Mn}_2\text{O}_3$ , which is tetragonal spinel with  $c/a = 1.16$ , is composed of  $\text{MnO}\cdot\text{MnO}_2$  with a similar ordering of  $\text{Mn}^{+4}$  and  $\text{Mn}^{+2}$  ions on the octahedral sites.

2. G. Aminoff, "Über die Kristallstruktur von Hausmannite ( $\text{MnMn}_2\text{O}_4$ )" Z. Krist. 64, 475-90 (1926).
3. E. J. Verwey and J. H. de Boer, "Cation Arrangement in a Few Oxides with Crystal Structures of the Spinel Type," Rec. Trav. Pays-Bas 55, 531-54 (1936).
4. E. J. Verwey et al., "Die Verteilung der Metallionen im Spinellgitter und deren Einfluss auf die Physikalischen Eigenschaften," Z. Physik. Chem. 198, 6-22 (1951).
5. E. J. Verwey, P. W. Haayman, and F. C. Romeijn, "Physical Properties and Cation Arrangements of Oxides with Spinel Structures: II. Electronic Conductivity," J. Chem. Phys. 15, 181-187 (1947).
6. J. B. Goodenough and A. Loeb, "Ordering in Manganese Oxides with Spinel Structure", Digital Computer Laboratory Memorandum M-2474, October 22, 1953.

Mason<sup>7</sup> has made a study of the variation of lattice parameters with composition in the  $\text{Fe}_3\text{O}_4$ - $\text{Mn}_3\text{O}_4$ - $\text{ZnMn}_2\text{O}_4$ - $\text{ZnFe}_2\text{O}_4$  system. His measurements of  $c/a$  and his phase diagram for this system are reproduced in Figures 1 and 2. The iron-rich portion of the two-phase region (Vredenburgite) is reported to consist of a lamellar precipitation of  $\text{Mn}_3\text{O}_4$  in a cubic matrix. A mechanism for the formation of this lamellar precipitate is now proposed.

It is assumed that Manganese is present in the spinel systems as  $\text{Mn}^{+2}$  and  $\text{Mn}^{+4}$ . It is further proposed that distortions of the lattice from cubic to tetragonal symmetry are the result of an ordering of the  $\text{Mn}^{+4}$  ions into every other plane parallel to a  $c$  axis. Since all three cubic axes have an equal probability of becoming a  $c$  axis, twinning results along  $\{101\}$  planes of the lattice in order to relieve the internal stresses which result. Such a twinning surface is shown diagrammatically in Figure 3(a). After twinning has occurred, the twinning surface becomes a region of low stress. Therefore there is a stress gradient on the odd-sized  $\text{Mn}^{+4}$  ions to cause them to diffuse toward the region of low stress. This gradient is proportional to  $eE/a$  where  $E$  is Young's modulus and the strain  $e$  is given by  $c/a = (1+e)$ . Diffusion of the  $\text{Mn}^{+4}$  ions toward the twinning surface will stop when the bulk matrix becomes cubic and  $e = 0$ . If the spinel lattice is maintained,  $\text{M}^{+2}$  ions must diffuse with the  $\text{Mn}^{+4}$  ions in order to maintain local electrical neutrality. It is assumed that cubic and tetragonal spinels are the only lattice types present. In Figure 3(b) is shown a diagram of the B-site lattice after precipitation is complete. Tetragonal  $2\text{MnO} \cdot \text{MnO}_2$  has precipitated at the twinning surface with its  $c$  axis in a  $[\bar{1}01]$  direction parallel to the  $\{101\}$  twinning surface. The bulk matrix becomes cubic when precipitation is complete. If precipitation is not complete, the bulk matrix is tetragonal, but its  $c/a$  ratio is smaller than that of the precipitate.

In support of this mechanism of lamellar precipitate formation, lattice-dimension and phase measurements for three compositions, marked R, S, BB in Figure 2, are taken from Mason's work and recorded in Table I. At compositions R and BB precipitation is not completed until lower temperatures are reached. Each of these cases is on the Manganese-rich side of the two-phase

7. B. Mason, "Minerological Aspects of the System  $\text{Fe}_3\text{O}_4$ - $\text{Mn}_3\text{O}_4$ - $\text{ZnMn}_2\text{O}_4$ - $\text{ZnFe}_2\text{O}_4$ ," American Mineralogist 32, 426-40 (1947).

region where considerable precipitation must occur before the parent matrix can become cubic. This view is quite consistent with the fact that the temperature range over which precipitation occurs increases with Manganese content. It is significant that the tetragonal phase of smaller c/a ratio becomes cubic. Composition BB shows a continuous decrease in the c/a ratio of the parent lattice until it becomes cubic whereas there is little change in the c/a ratio of the precipitate. This is just the behavior predicted by the proposed precipitation mechanism.

Table I

Prep.	Composition				Phases	Cubic				Remarks
	Fe	Mn	Zn	T		a	a	c	c/a	
R	16.7	50.0	33.3	890	T		8.162	8.991	1.102	Brackets indicate small amount
				800	T+(T <sub>1</sub> )		(8.120)	9.107	1.121	
				710	T+(c)	(8.423)	(8.204)	(8.872)	(1.081)	
				590	T+(c)	(8.422)	8.114	9.115	1.123	
							8.111	9.139	1.127	
S	26.7	40.0	33.3	920	T		8.217	8.869	1.080	
				810	T		8.214	8.861	1.079	
				700	C+T	8.424	8.125	9.099	1.120	
				600	C+T	8.422	8.117	9.121	1.124	
BB	18.8	56.2	25	1000	T		8.181	9.065	1.108	Brackets indicate small amount
				920	T+T <sub>1</sub>		(8.138)	9.143	1.124	
							(8.183)	(9.025)	(1.103)	
				810	T+T <sub>1</sub>		(8.137)	9.136	1.123	
							(8.212)	(8.953)	(1.090)	
			710	T+T <sub>1</sub>		(8.133)	9.136	1.123		
						(8.250)	(8.934)	(1.083)		
			600	C+T	8.433	8.129	9.169	1.128		

### III. Prediction of Compositions with Square B-H Loops

If lamellar  $2\text{MO}\cdot\text{MnO}_2$  is readily formed in a spinel system which is rich in  $\text{Mn}^{+4}$  and if the presence of extensive lamellar precipitation prevents the occurrence of a square B-H loop, as has been proposed, it should be possible to predict in which compositional regions of the  $\text{MgO}\text{-Fe}_2\text{O}_3\text{-MnO}$  system square B-H loops are attainable. If, further, there were information available on the variations of  $K$ ,  $A$ , and  $I_s$  with composition, it should be possible to predict an optimum compositional value. This latter accomplishment must await measurements of the physical constants. A rough prediction of the general regions in which optimum core characteristics are to be found can, however, be made on the basis of our present knowledge.

It is known experimentally that in any spinel certain ions prefer the four coordination of a tetrahedral site. The order of preference for ions which are significant to this discussion is  $\text{Zn}^{2+}$ ,  $\text{Fe}^{3+}$ ,  $\text{Mg}^{2+}$ . This order of preference has little to do with the ion size. Rather it is due to the strength of the covalent bonding between the oxygen ions and the cation in a tetrahedral site. Hybridization of ( $d^3s$ ) orbitals<sup>8</sup> gives four electron orbitals which point to the corners of a tetrahedron. The  $\text{Zn}^{2+}$  ion characteristically forms covalent bonds with the tetrahedral coordination. The  $\text{Fe}^{3+}$  ion can also readily hybridize ( $d^3s$ ) orbitals to enter into covalent bonds of tetrahedral symmetry. However, that  $\text{ZnOFe}_2\text{O}_3$  forms a normal spinel shows  $\text{Zn}^{2+}$  to have the stronger preference for the tetrahedral site. In the  $\text{Mg}^{2+}$  ion ( $r^3s$ ) orbitals can be hybridized. These have the tetrahedral symmetry which is necessary for covalent bonding in a tetrahedral site. The energy of the s state is sufficiently above the p-state energies, however, that a smaller amount of energy is gained through this admixture of states than through the admixture of ( $d^3s$ ) states in  $\text{Fe}^{3+}$ . This is evidenced by the fact that  $\text{MgO}\cdot\text{Fe}_2\text{O}_3$  is mostly inverse spinel.<sup>9</sup> It is concluded, therefore, that in a spinel lattice in which  $\text{Zn}^{2+}$ ,  $\text{Fe}^{3+}$ , and  $\text{Mg}^{2+}$  ions are present, the tetrahedral, or A, sites will be occupied by the  $\text{Zn}^{2+}$  ions.

8. G. E. Kimball, "Directed Valence," J. Chem. Phys. 8, 188-98 (1940).

9. L. M. Corliss, J. M. Hastings, and F. G. Brockman, "Neutron Diffraction Study of Magnesium Ferrite," Phys. Rev. 90, 1013-18 (1953).

Memorandum M-2473

Page 7 of 10

If there are still some vacant A sites, these will be predominately occupied by  $\text{Fe}^{3+}$  ions. The  $\text{Mg}^{2+}$  ions will be assumed, in the arguments to follow, to occupy the octahedral, or B, sites.

If manganese is present in the system, the  $\text{Mn}^{2+}$  ion, which has the same outer electron configuration as  $\text{Fe}^{3+}$ , will also have a preference for covalent bonding in the tetrahedral site. Since  $\text{MnO}\cdot\text{Fe}_2\text{O}_3$  appears to be an inverse spinel,<sup>10</sup> it is concluded that the  $\text{Fe}^{3+}$  ions have the greater preference for the A sites. In the considerations which follow, all  $\text{Mn}^{2+}$  ions will be considered to occupy B sites unless there are not sufficient  $\text{Zn}^{2+}$  or  $\text{Fe}^{3+}$  ions to fill the A sites. The  $\text{Fe}^{2+}$  ion, with six outer electrons, can form a six-fold covalent coordination. It will be considered to always occupy B sites as it does in magnetite ( $\text{Fe}_3\text{O}_4$ ). The  $\text{Mn}^{4+}$  ion will also be considered to always occupy B sites as it does in Hausmannite ( $\text{Mn}_3\text{O}_4$ ).<sup>6</sup>

Just as the tetragonality of  $\text{Mn}_3\text{O}_4$  and  $\gamma\text{-Mn}_2\text{O}_3$  is attributed to an ordering of the  $\text{Mn}^{4+}$  ions into every other plane of B sites parallel to a c axis, so it is proposed that tetragonality in any spinel system containing manganese is due to a similar ordering of  $\text{Mn}^{4+}$  ions. A fraction  $f$  will be defined as the fraction of  $\text{Mn}^{4+}$  ions per B site which are necessary before ordering occurs. Since distortions to tetragonality introduce twinning planes at which the precipitation of  $2\text{MO}\cdot\text{MnO}_2$  can occur, this fraction  $f$  will also be the critical fraction for lamellar precipitate formation. If the fraction of  $\text{Mn}^{4+}$  ions per B site exceeds  $f$ , the B-H loop will not be square. The lamellar precipitates will be acting as nucleating centers for domains of reverse magnetization, and  $H_n < H_c$ .

Although the valencies of both the manganese and the iron ions may be variable, a minimum value of  $f$  can be obtained from Mason's<sup>7</sup> work. If the iron ions are all  $\text{Fe}^{3+}$  in the  $\text{ZnFe}_2\text{O}_4\text{-ZnMn}_2\text{O}_4$  composition at which tetragonality sets in,  $f$  can be calculated from Figure 1. The unit cell contains 8  $\text{Zn}^{2+}$  on the A sites and 3.1  $\text{Mn}^{4+}$  3.1  $\text{Mn}^{2+}$  9.8  $\text{Fe}^{3+}$  on the B sites. This gives  $f = 3.1/16$ . In the  $\text{Fe}_3\text{O}_4\text{-Mn}_3\text{O}_4$  system, the highest manganese content at which tetragonality first occurs is 60 mol percent  $\text{Mn}_3\text{O}_4$ . If all of the iron ions are  $\text{Fe}^{3+}$  at this composition, the unit cell contains 8  $\text{Fe}^{3+}$  on the A sites and 1.6  $\text{Fe}^{3+}$  3.2  $\text{Mn}^{4+}$  11.2  $\text{Mn}^{2+}$  on the B sites. This gives an  $f = 1/5$ . The value  $f = 1/5$  is therefore taken as the critical fraction of  $\text{Mn}^{4+}$  ions per B site. If a

10. E. J. W. Verwey and E. L. Heilmann, "Physical Properties and Cation Arrangement of Oxides with Spinel Structures; I. Cation Arrangement in Spinel," J. Chem. Phys. 15, 174-180 (1947).

Memorandum M-2473

Page 8 of 10

greater concentration of  $Mn^{4+}$  ions is present, lamellar precipitate will presumably be present. The B-H loop is predicted to be nonsquare for these compositions.

The ternary diagram of Figure 4 is marked off into five compositional regions. In Region I MgO will precipitate. It is probable that  $Fe_2O_3$  precipitates in Region II. The nature of these precipitates is not yet known. Suffice it to say that the presence of precipitation in these regions may be expected to destroy the squareness of the B-H loop. In Region III  $f > 1/5$  regardless of the degree of ionization of the iron atoms. This will therefore be a two-phase region in which tetragonal  $2MnO_2$  forms a lamellar precipitate along  $\{101\}$  surfaces of a cubic matrix. Materials of these compositions will form magnetic cores with nonsquare B-H loops unless they are rapidly quenched from a temperature above the ordering temperature. A rapid quench may succeed in "freezing in" the disordered arrangement of  $Mn^{4+}$  ions. The disordered lattice will be cubic, and the precipitation mechanism will not exist. In Region IV  $f < 1/5$  regardless of the degree of ionization of the iron atoms. This represents the region of complete miscibility. The single phase will be cubic, and the B-H loops of cores made from these compositions should have good squareness. The boundary between Regions IV and V represent  $f = 1/5$  if all the manganese present is  $Mn^{4+}$ . Region V is the compositional region in which the B-H loop shape will be sensitive to firing and annealing conditions.

The magnitude of  $f$  can be critically controlled in Region V by the firing and annealing atmospheres used. In an oxygen-rich atmosphere there will be a tendency to form  $Mn^{4+}$  ions. If the spinel lattice is maintained, this may be accomplished by a transfer of electrons from an  $Mn^{2+}$  to two  $Fe^{3+}$  ions to give an  $Mn^{4+}$  and two  $Fe^{2+}$  ions. More probably, however, the lattice becomes cation deficient as oxygen is added to the lattice. For every oxygen added, an  $Mn^{2+}$  becomes  $Mn^{4+}$  and a normally-occupied B site becomes vacant.

It has been found experimentally that if a material of composition in Region V is fired in air, the atmosphere is sufficiently rich in oxygen for lamellar precipitation to form. These lamellar precipitates are removed either by quenching rapidly from above the ordering temperature or by annealing in an oxygen-free atmosphere above  $1000^\circ C$ . In the latter process oxygen ions are removed from the lattice and enough  $Mn^{4+}$  ions become  $Mn^{2+}$  to make  $f < 1/5$ . Temperatures in excess of  $1000^\circ C$  are sufficient, according to



Memorandum M-2473

Page 9 of 10

Mason's data, for the  $Mn^{4+}$  ions to diffuse away from a twinning surface at which precipitation has occurred. Since there are no longer sufficient  $Mn^{4+}$  ions present to give ordering, the lattice is cubic, and there is no precipitate at room temperature.

It should be noted that some reducing atmospheres may reduce the  $Fe^{3+}$  ions to  $Fe^{2+}$  and thus force some  $Mn^{2+}$  ions to become  $Mn^{4+}$ . Controlled oxygen atmospheres may be necessary for optimum conditions.

Finally one can predict an electrical conductivity approaching that of magnetite in those samples which contain disordered  $Fe^{2+}$ ,  $Fe^{3+}$  ions on the B sites. This conductivity will be due to the exchange of electrons between like atoms of different degrees of ionization. The exchange between  $Mn^{2+}$  and  $Mn^{4+}$  ions will give a lower contribution to the conductivity.<sup>6</sup>

#### IV. Comparison with Preliminary Experiments

##### A. Best Squareness Ratios vs. Composition

The chemistry section of Group 63, under the direction of F. E. Vinal, has prepared ferrite cores of a large number of different compositions within the  $MgO-Fe_2O_3-Mn_3O_4$  system. Each composition was fired in air at  $1300^{\circ}C$ ,  $1350^{\circ}C$ ,  $1400^{\circ}C$ ,  $1450^{\circ}C$  and refired in  $N_2$  at  $1100^{\circ}C$ . In Figure 5 is a contour map for the best squareness ratios at each composition. In Figure 6 is shown a contour map of the average change in squareness with refiring. The following conclusions are at once apparent.

1. The compositions of favorable squareness lie within Regions IV and V as predicted.
2. The compositions which are sensitive to anneal in an oxygen-free atmosphere lie in Region V as predicted.
3. The lower squareness compositions within Region V are manganese-rich samples which failed to respond appreciably to an anneal in an oxygen-free atmosphere. It is believed that improved squareness can be obtained in these regions.

##### B. Microstructure Studies

Some microstructures have been prepared by the chemistry section of Group 63 and by A. Kulin of Group 35. These studies have shown lamellar precipitation in air-fired samples of Region V. This precipitate is most

commonly found near the surface of the material or at flaws. A typical micrograph for such a region is shown in Figure 7. It corresponds to the composition marked A in Figures 5 and 6. For four materials of this composition originally fired in air at 1300°C, 1350°C, 1400°C, 1450°C, the average increase in squareness ratio with refire in Nitrogen was 0.27.

The General Ceramics Corp. MF-1371 body is located in Region V. The micrograph and B-H loop for an air-fired and steam-fired specimen of this material are shown in Figure 8. Extensive lamellar precipitation is apparent. The precipitation pattern is strongly suggestive of a heavy twinning pattern. Such a precipitate pattern is predicted by Section II and Section III.

C. Miscellaneous


The Group 63 chemistry staff has found that some cores of the 7.5 percent iron-deficient series in the  $\text{MgO-Fe}_2\text{O}_3\text{-MnO}$  system are difficult to press and to fire. These compositions are all located in Region V. The raw oxides are first reacted in air at elevated temperatures to allow shrinkage to occur. The product is reground and then pressed into cores for the final firing. Mason<sup>7</sup> found that a material in which lamellar precipitation had just begun crumbled to pieces on handling because of the presence of large internal strains. It is suggested, therefore, that sufficient oxydation of the manganese has occurred during the initial reacting process for precipitation to have begun. If this is true, the difficulty may be removed by reacting the materials initially in an inert atmosphere.

I should like to express my appreciation to F. E. Vinal for access to his data which is yet in incomplete compilation.

Signed

  
John B. Goodenough

Approved

  
David R. Brown

JBG/jk

Drawings attached:

Figures 1, 2 A-56625	Figure 5 A-56628
Figure 3 A-56626	Figure 6 A-56629
Figure 4 A-56627	Figure 7 A-56630
	Figure 8 A-56064

cc: Group 63 staff  
S. Foner - Group 37

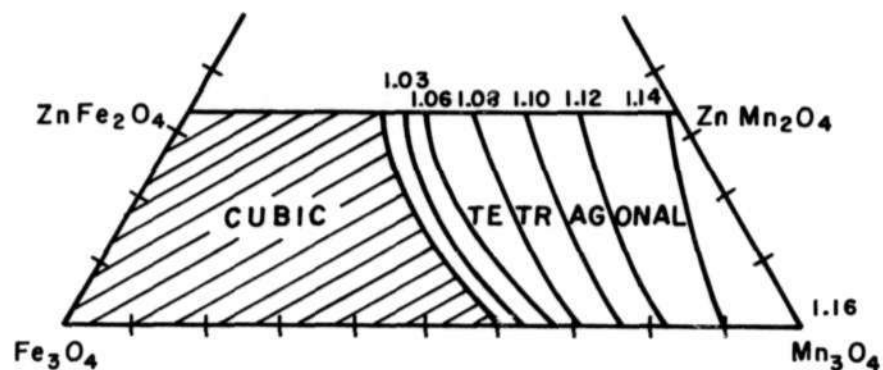


FIG.1  
 VARIATION OF THE AXIAL RATIO  $c/a$  WITH COMPOSITION.

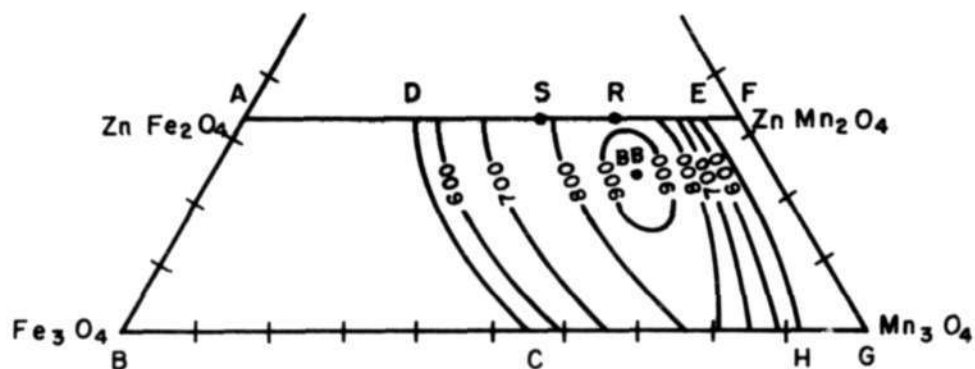
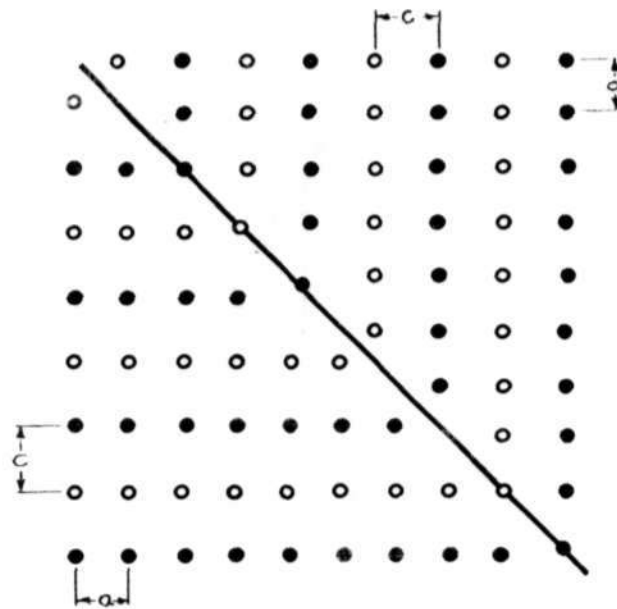
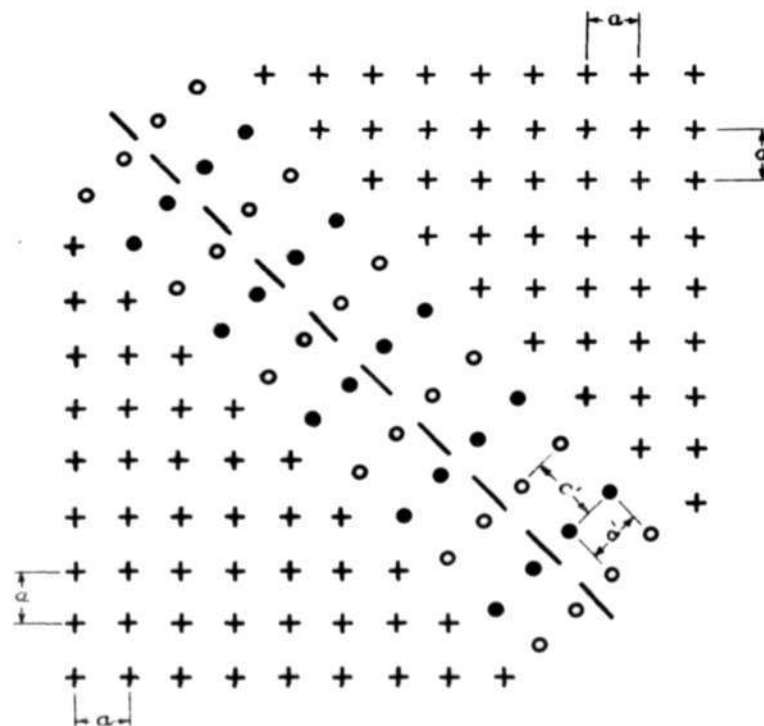


FIG.2  
 ABCD IS THE FIELD OF CUBIC MIX-CRYSTALS. EFGH IS THE FIELD OF TETRAGONAL MIX-CRYSTALS. CDEH IS THE FIELD OF INCOMPLETE MISCIBILITY; ISOTHERNS SHOW THE BOUNDARIES OF THE FIELD OF INCOMPLETE MISCIBILITY AT DIFFERENT TEMPERATURES.



(a)

B SITES IN A DISTORTED SPINEL LATTICE IN THE REGION OF A {101} TWINNING SURFACE. DARK SITES ARE THOSE WHICH MAY BE OCCUPIED BY Mn<sup>4+</sup> IONS

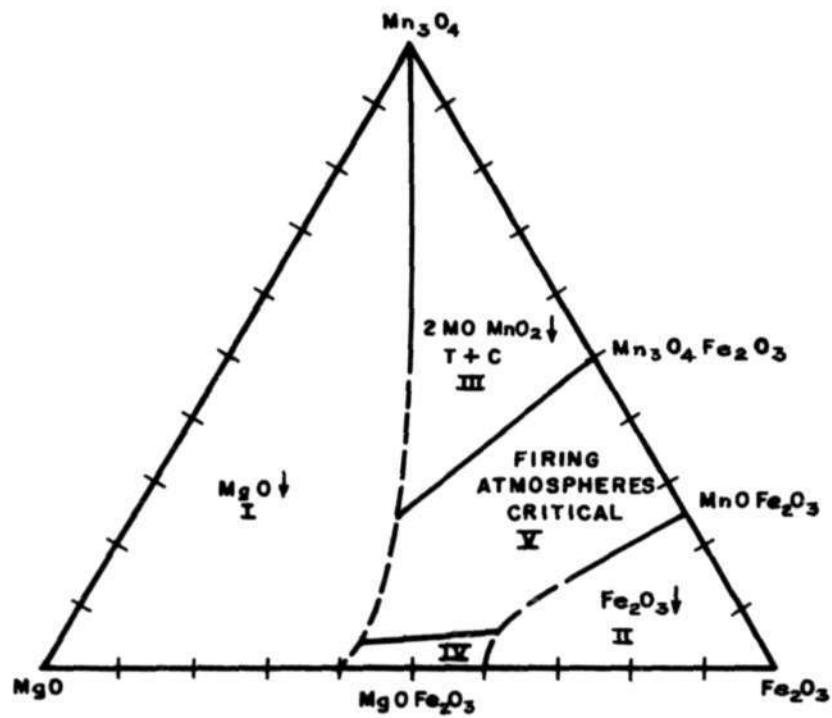


(b)

B SITES AFTER PRECIPITATION IS COMPLETE. DARK SITES ARE OCCUPIED BY Mn<sup>4+</sup> IONS

FIG. 3

DIAGRAMATIC REPRESENTATION OF PRECIPITATE FORMATION AT A TWINNING SURFACE



REGIONS I, II, III GIVE POOR SQUARENESS.  
 REGION IV FAVORABLE TO GOOD SQUARENESS.  
 REGION V FAVORABLE TO GOOD SQUARENESS  
 PROVIDED ALL FIRING PROCESSES ARE DONE  
 IN A REDUCING ATMOSPHERE.

FIG. 4  
 PREDICTED COMPOSITIONAL REGIONS OF HIGH  
 AND LOW B-H LOOP SQUARENESS

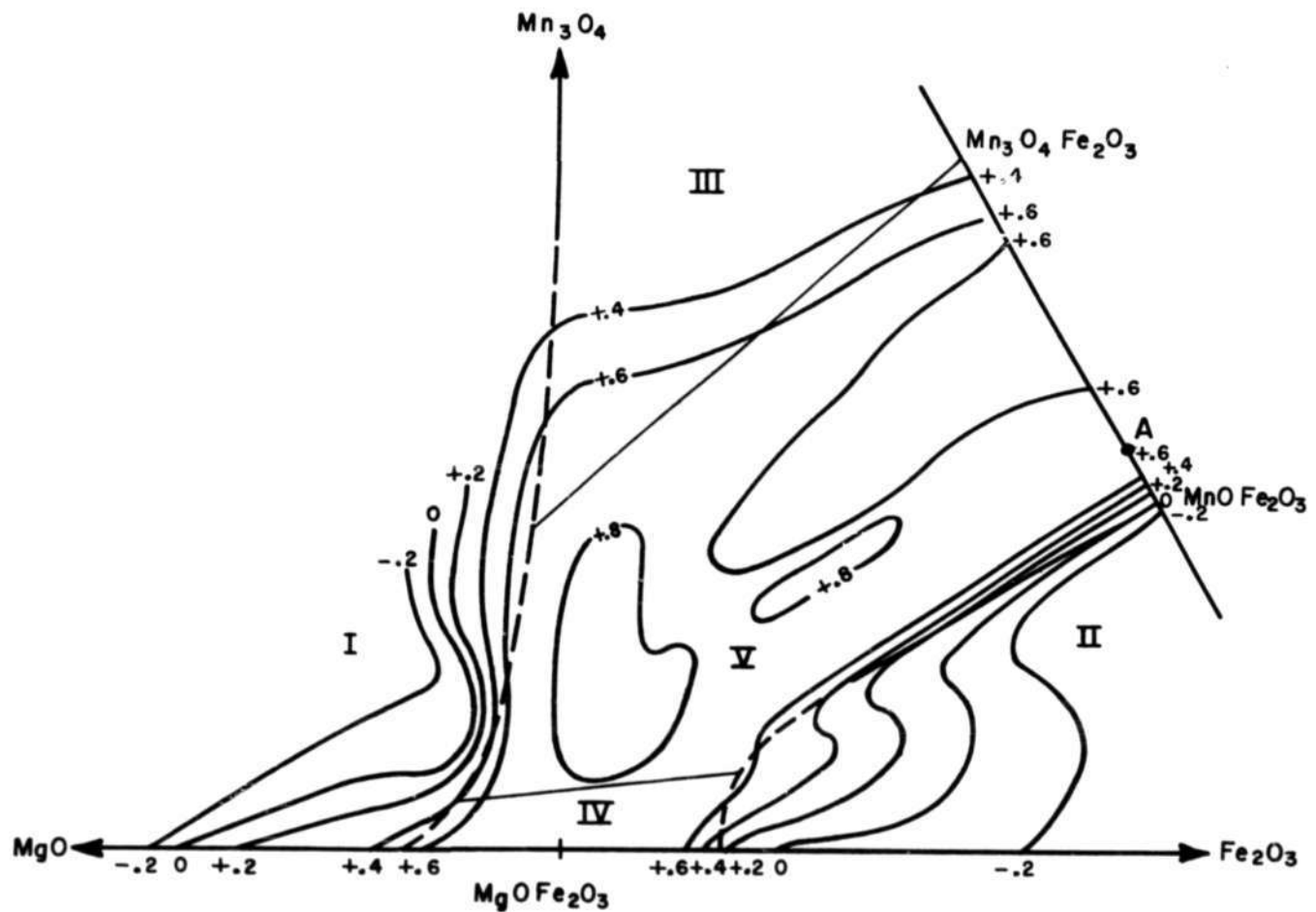


FIG. 5

CONTOURS OF HIGHEST SQUARENESS RATIO  $R_s = B_m/B_d$   
WHICH HAVE BEEN OBTAINED TO DATE UNDER VARIOUS  
FIRING AND PROCESSING CONDITIONS.

A-56628

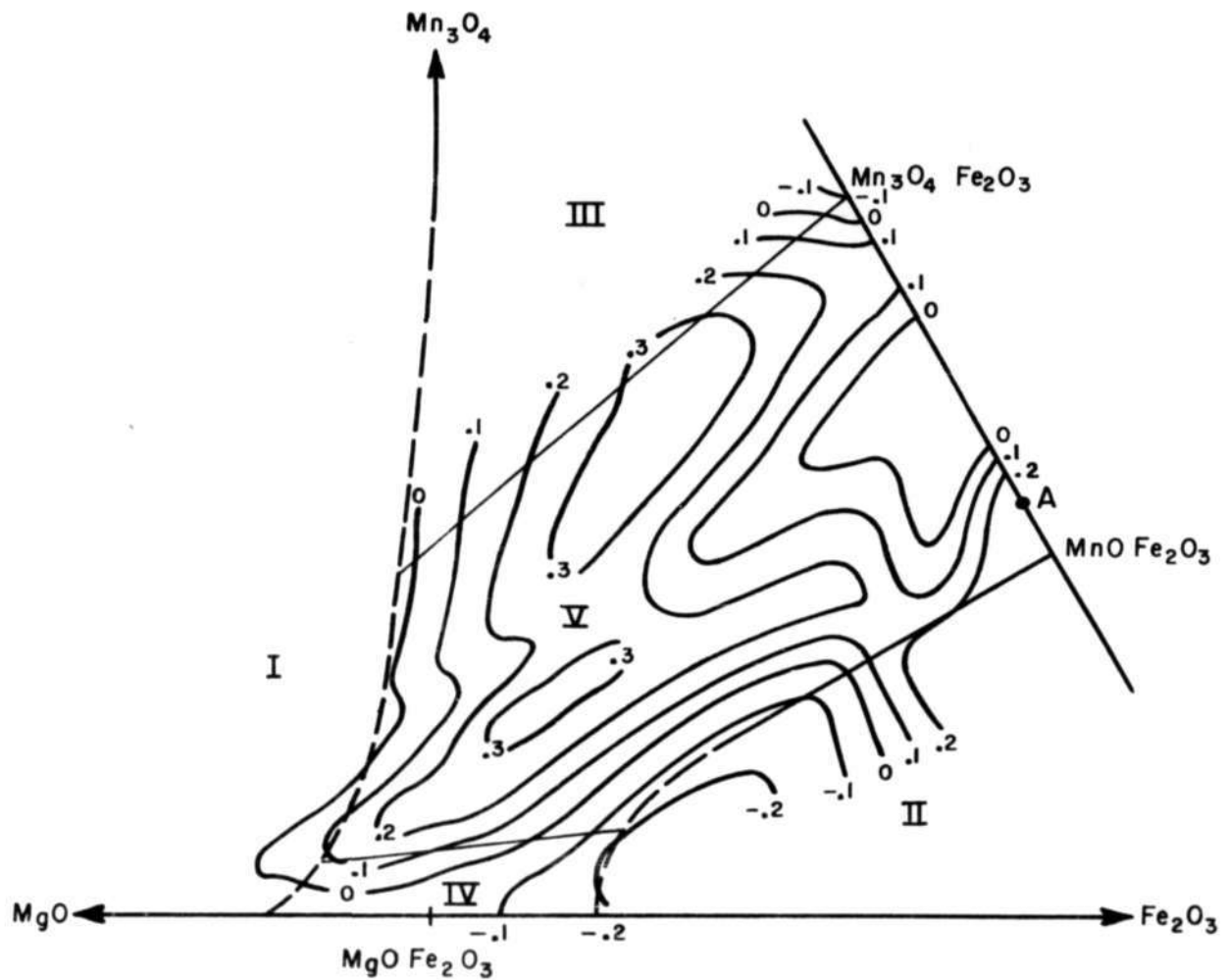


FIG. 6

CONTOURS OF AVERAGE CHANGE IN  $R_5$  AFTER RE FIRING CORES FOR ONE HOUR AT  $1100^{\circ}C$  IN AN  $N_2$  ATMOSPHERE. THE CORES WERE ORIGINALLY FIRED IN AIR FOR ONE HOUR AT  $1300^{\circ}C$ ,  $1350^{\circ}C$ ,  $1400^{\circ}C$ , AND  $1450^{\circ}C$ .

A - 56629



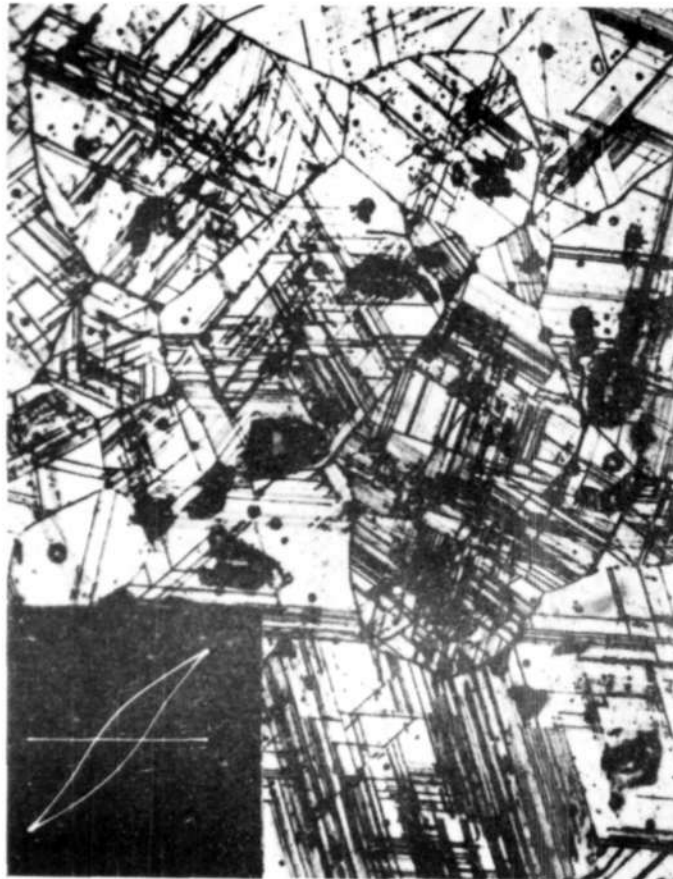
FIG. 7

TYPICAL LAMELLAR PRECIPITATE FORMATION IN  
55 mol % MnO 45 mol %  $Fe_2O_3$ . OXIDES WERE  
SINTERED IN AIR FOR ONE HOUR AT 1400° C.  
(WHITE LIGHT X167)

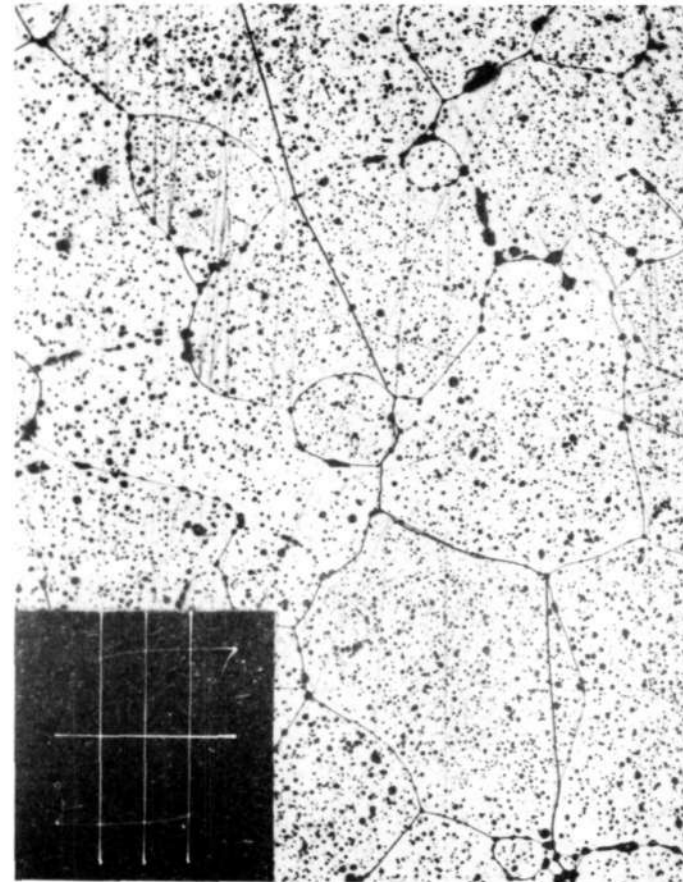
A - 56630



A-56064



(a)  $B_m = 150$  GAUSS  
 $H_m = 2.25$  Oe



(b)  $B_m = 1128$  GAUSS  
 $H_m = 0.46$  Oe

FIG. 8

MICROSTRUCTURE AND MAXIMUM SQUARENESS RATIO  
B-H LOOP FOR A GENERAL CERAMIC CO.  
MF 1371B FERRITE BODY (a) BEFORE ANNEAL (WHITE LIGHT  
X 498) AND (b) AFTER ANNEAL (WHITE LIGHT X 100)